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Second Law of Thermodynamics

By: S K Mondal

Chapter 6

If this system is used as a heat pump, how many MJ of heat would be available for heating for each MJ of heat input to the engine?

(Ans. 1.8 MJ)

Solution:

COP of the Ref. is 5

So for each MJ removed from the cold body we need work

$$= \frac{1 \text{ MJ}}{5} = 200 \text{ kJ}$$

For 200 kJ work output of heat engine heat $\eta = 30\%$

We have to supply heat $= \frac{200 \times 100}{30} = 666.67 \text{ kJ}$

Now

COP of H.P. = COP of Ref. + 1

$$= 5 + 1 = 6$$

Heat input to the H.P. = 1 MJ

Work output (W) = 1 + 0.2 MJ = 200 kJ

That will be the input to H.P.

$$= (\text{COP})_{\text{H.P.}} \times \frac{W}{6}$$
$$= 6 \times 200 \text{ kJ} = 1.2 \text{ MJ}$$

Q8.4

An electric storage battery which can exchange heat only with a constant temperature atmosphere goes through a complete cycle of two processes. In process 1-2, 2.8 kWh of electrical work flow into the battery while 70 kJ of heat flow out to the atmosphere. During process 2-1, 2.4 kWh of work flow out of the battery.

(a) Find the heat transfer in process 1-1.

(b) If the process 1-2 has occurred as above, does the first law as the second law limit the maximum possible work of process 2-1? What is the maximum possible work?

(c) If the maximum possible work were obtained in process 2-1, what will be the heat transfer in the process?

(Ans. (a) = 700 kJ (b) Second law, $W_{12} = 8248 \text{ kJ}$ (c) $Q_{12} = 0$)

Solution:

From the first Law of thermodynamics

(a) For process 1-2

$$Q_{12} = E_2 - E_1 + W_{12}$$
$$= 712 - (E_2 - E_1) = 10000$$
$$= 2.8 \text{ kWh} = 2.8 \times 3600 \text{ kJ}$$
$$= E_2 - E_1 = 8144 \text{ kJ}$$

For process 2-1

$$Q_{21} = E_1 - E_2 + W_{21}$$
$$= -8144 + 8640$$
$$= -504 \text{ kJ}$$

Heat flow out to the atmosphere.

(b) Yes Second Law limits the maximum possible work. As Electric energy stored in a battery is High grade energy so it can be completely converted to the work. Then

$$W = 8144 \text{ kJ}$$

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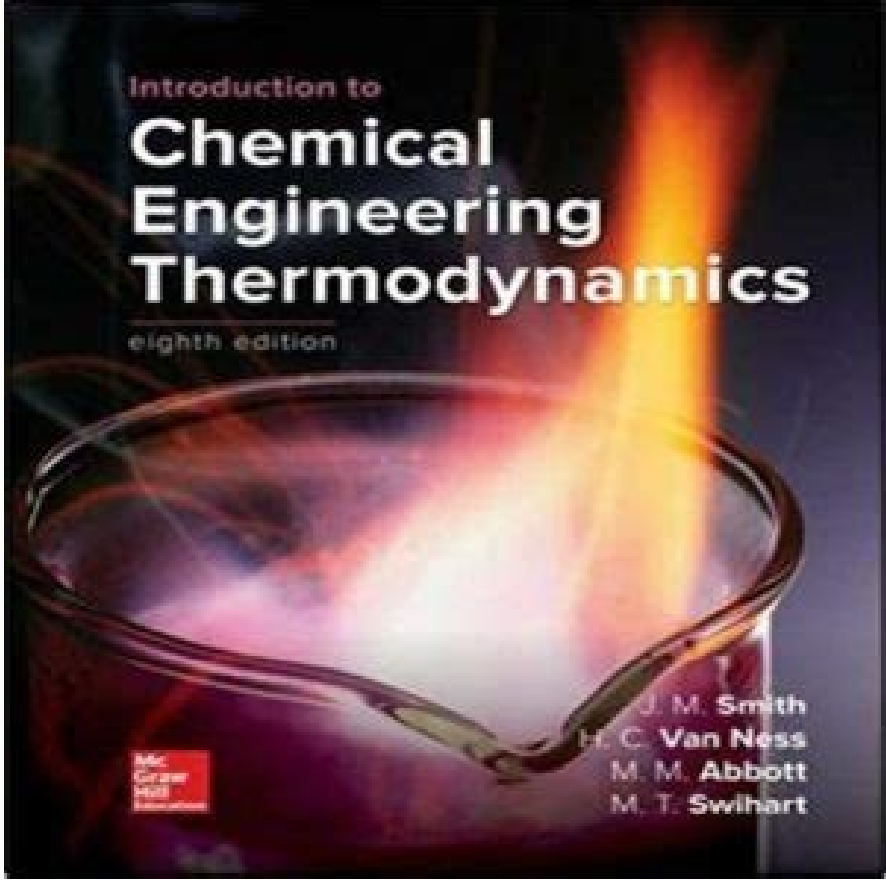
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A far higher problem is to develop the capability to cause within the context of thermodynamics in order that one can apply thermodynamic rules within the answer of sensible issues. 3 Kinetic and potential energy changes are negligible. The second regulation is developed in Chap. 9 kJ/kg (1.669 kg/s) 2 (300 K) (7.101 7.117)kJ/kg.K 1 kJ/kg 1000 m 2 /s 2 12.4 kW (c) The second-law efficiency for this device may be defined as the exergy output divided by the exergy input: $\dot{V}_2 X_1 m \dot{h}_1 \dot{h}_0 1 \dot{T}_0 (\leq 1 \leq 0) 2 (205 \text{ m/s}) 2 1 \text{ kJ/kg} (1.669 \text{ kg/s})(88.39 1.93) \text{ kJ/kg} 2 1000 \text{ m} 2 /s 2 (300 \text{ K})(7.101 6.846) \text{ kJ/kg.K} 51.96 \text{ kW} \text{ II } X X 2 12.4 \text{ kW} 1 \text{ dest } 1 0.761 76.1\% 51.96 \text{ kW } X 1 X 1 \text{ PROPRIETARY MATERIAL. 6-32C The coefficient of performance of a refrigerator represents the amount of heat removed from the refrigerated space for each unit of work supplied. The purpose of a refrigerator is to remove heat from a cold medium whereas the purpose of a heat pump is to supply heat to a warm medium. There is no creation of energy, and thus no violation of the conservation of energy principle. Analysis Using variable specific heats, the properties can be determined using the air table as follows u } 214.07 \text{ kJ/kg} 0 0 \text{ T1 } \text{ T2 } 300 \text{ K } \leq 1 \leq 2 1.70203 \text{ kJ/kg.K } \text{ P } 1 \text{ Pr } 2 1.3860 \text{ T} = \text{const. 6-30C No. Because the refrigerator consumes work to accomplish this task. 1-kg-force is the force required to accelerate a 1-kg mass by } 9.807 \text{ m/s}^2 \text{. energies WATER } 0 \text{ U or, Copper } 50 \text{ kg Ucu U water } 0 [\text{mc(T2 } \text{T1)}] \text{Cu } [\text{mc(T2 } \text{T1)}] \text{water } 0 90 \text{ L where mwater } \text{V } (997 \text{ kg/m}^3 (0.090 \text{ m } 3) 89.73 \text{ kg Using specific heat values for copper and liquid water at room temperature and substituting, } (50 \text{ kg})(0.386 \text{ kJ/kg } \text{C})(\text{T2 } 140\text{C } (89.73 \text{ kg}) (4.18 \text{ kJ/kg } \text{C})(\text{T2 } 10\text{C } 0 \text{ T2 } = 16.4\text{C} = 289.4 \text{ K The entropy generated during this process is determined from T } 289.4 \text{ K } 8.864 \text{ kJ/K } \text{S copper } \text{mc avg ln } 2 50 \text{ kg } 0.386 \text{ kJ/kg } \text{K ln } 413 \text{ K } \text{T1 } \text{T } 289.4 \text{ K } 8.388 \text{ kJ/K } \text{S water } \text{mc avg ln } 2 89.73 \text{ kg } 4.18 \text{ kJ/kg } \text{K ln } 283 \text{ K } \text{T1 } \text{Thus, S total } \text{S copper } \text{S water } 6.864 8.388 1.52 \text{ kJ/K } \text{PROPRIETARY MATERIAL. } \text{C } 2015 \text{ McGraw-Hill Education. 2 The system is stationary and thus the kinetic and potential energies are negligible. kJ } \text{kg s10 } 1.66802 \text{ kJ } \text{kg } \text{K T2 } 440 \text{ K } 600 \text{ kPa } 167\text{C h2 } 441.61 \text{ kJ } \text{kg s20 } 2.0887 \text{ kJ } \text{kg } \text{K Analysis The increase in exergy is the difference between the exit and inlet fluid exergies. AIR } 8 \text{ kW Increase in exergy } 2 1 0.0 (\text{h2 } \text{h1}) \text{ke } \text{pe } \text{T0 } (\leq 2 \leq 1) (\text{h2 } \text{h1}) \text{T0 } (\leq 2 \leq 1) 100 \text{ kPa } 17\text{C where } \text{P2 } \text{P1 } 600 \text{ kPa } (2.0887 1.66802) \text{ kJ/kg } \text{K } (0.287 \text{ kJ/kg } \text{K}) \text{ln } 100 \text{ kPa } 0.09356 \text{ kJ/kg } \text{K s } 2 \leq 1 (\leq 20 \leq 10) \text{ R ln Substituting, Increase in exergy } 2 1 (441.61 290.16) \text{ kJ/kg } (290 \text{ K})(0.09356 \text{ kJ/kg } \text{K}) 178.6 \text{ kJ/kg Then the reversible power input is } (2 1) (2.1 / 60 \text{ kg/s})(178.6 \text{ kJ/kg}) 6.25 \text{ kW W rev.in m (b) The rate of exergy destruction (or irreversibility) is determined from its definition, X destroyed } \text{W in } \text{W rev.in } 8 6.25 1.75 \text{ kW Discussion Note that } 1.75 \text{ kW of power input is wasted during this compression process. Analysis Applying Newton's second law, the weight is determined to be } \text{W } \text{mg } (200 \text{ kg})(9.6 \text{ m/s } 2) 1920 \text{ N } 1\text{-10 A plastic tank is filled with water. Certainly, there is no such thing as a approach to make it easy. The height at which the weight of a body will decrease by } 0.3\% \text{ is to be determined. The place solely a single-semester course in chemical engineering thermodynamics is offered, these chapters might symbolize adequate content material. Download full file from buklibry.com Full file at 7-33 Entropy Change of Incompressible Substances 7-59C No, because entropy is not a conserved property. (Similar problems and their solutions can be obtained easily by modifying numerical values). 3 Nitrogen is an ideal gas with variable specific heats. Download full file from buklibry.com Full file at 1-2 Thermodynamics 1-1C Classical thermodynamics is based on experimental observations whereas statistical thermodynamics is based on the average behavior of large groups of particles. Though introductory in nature, the fabric of this textual content shouldn't be thought of easy. 6-33C The coefficient of performance of a heat pump represents the amount of heat supplied to the heated space for each unit of work supplied. Furthermore, we go al to encourage understanding by writing in easy active-voice, present-tense prose. Assumptions 1 Air is an ideal gas with variable specific heats. Properties The gas constant of air is $R = 0.287 \text{ kPa}\cdot\text{m}^3/\text{kg}\cdot\text{K}$ (Table A-1). "Given" $T_1 = 298 \text{ [K]}$ $T_2 = 3000 \text{ [K]}$ " $P = 1 \text{ [atm]}$ " $m \dot{\text{m}} = 0.2 \text{ [kg/min]}$ $T_0 = 298 \text{ [K]}$ "The equilibrium constant for these two reactions at 3000 K $p_1 = \exp(-3.086) \text{ K}$ $p_2 = \exp(-2.937) \text{ "Properties" MM } \text{H}_2\text{O} = \text{molarmass}(\text{H}_2\text{O}) \text{ "Analysis" (a) "Actual reaction: } \text{H}_2\text{O} = \text{N } \text{H}_2\text{O } \text{H}_2\text{O} + \text{N } \text{O}_2 \text{O}_2 + \text{N } \text{OH OH" } 2\text{-2"N } \text{H}_2\text{O} + 2\text{"N } \text{H}_2 + \text{N } \text{OH "H balance" } 1 = \text{N } \text{H}_2\text{O} + 2\text{"N } \text{O}_2 + \text{N } \text{OH "O balance" N total} = \text{N } \text{H}_2\text{O} + \text{N } \text{H}_2 + \text{N } \text{O}_2 + \text{N } \text{OH "Stoichiometric reaction 1: } \text{H}_2\text{O} = \text{H}_2 + 1/2 \text{O}_2 "Stoichiometric coefficients for reaction 1" n } \text{H}_2\text{O } 1 = 1 \text{ n } \text{H}_2 1 = 1 \text{ n } \text{O}_2 1 = 1/2 "Stoichiometric reaction 2: } \text{H}_2\text{O} = 1/2 \text{H}_2 + \text{OH" "Stoichiometric coefficients for reaction 2" n } \text{H}_2\text{O } 2 = 1 \text{ n } \text{H}_2 2 = 1/2 \text{ n } \text{OH } 2 = 1 "K p relations are" K } p_1 = (\text{N } \text{H}_2^{\wedge} \text{nu } \text{H}_2 1^{\wedge} \text{N } \text{O}_2^{\wedge} \text{nu } \text{O}_2 1)/\text{N } \text{H}_2^{\wedge} \text{nu } \text{H}_2\text{O } 1^{\wedge} \text{P/N total})^{\wedge} \text{nu } \text{H}_2 1 + \text{nu } \text{O}_2 1 - \text{nu } \text{H}_2\text{O } 1) \text{ K } p_2 = (\text{N } \text{H}_2^{\wedge} \text{nu } \text{H}_2 2^{\wedge} \text{N } \text{OH } 2)/\text{N } \text{H}_2\text{O } 2^{\wedge} \text{nu } \text{H}_2\text{O } 2^{\wedge} \text{P/N total})^{\wedge} \text{nu } \text{H}_2 2 + \text{nu } \text{OH } 2 - \text{nu } \text{H}_2\text{O } 2) "Enthalpy of formation data from Table A-26" h } \text{f } \text{OH} = 39460 "Enthalpies of products" h } \text{H}_2\text{O } \text{R} = \text{enthalpy}(\text{H}_2\text{O, T} = \text{T1}) \text{ h } \text{H}_2\text{O } \text{P} = \text{enthalpy}(\text{H}_2\text{O, T} = \text{T2}) \text{ h } \text{H}_2 = \text{enthalpy}(\text{H}_2, \text{T} = \text{T2}) \text{ h } \text{O}_2 = \text{enthalpy}(\text{O}_2, \text{T} = \text{T2}) \text{ h } \text{OH} = 98763 "at T2 from the ideal gas tables in the text" "Standard state enthalpies" h } \text{o } \text{OH} = 9188 "at T0 from the ideal gas tables in the text" "Heat transfer" H } \text{P} = \text{N } \text{H}_2\text{O}^{\wedge} \text{h } \text{H}_2\text{O } \text{P} + \text{N } \text{H}_2^{\wedge} \text{h } \text{H}_2 + \text{N } \text{O}_2^{\wedge} \text{h } \text{O}_2 + \text{N } \text{OH } \text{OH" (h } \text{f } \text{OH} + \text{h } \text{OH} - \text{h } \text{O } \text{H } \text{R} = \text{N } \text{H}_2\text{O } \text{R}^{\wedge} \text{h } \text{H}_2\text{O } \text{R } \text{H}_2\text{O } \text{R} = 1 \text{ Q in a} = \text{H } \text{P} - \text{H } \text{R } \text{Q } \text{dot in a} = (\text{m } \text{dot}/\text{MM } \text{H}_2\text{O}^{\wedge} \text{Q in a " (b) "Q in b} = \text{N } \text{H}_2\text{O } \text{R}^{\wedge} (\text{h } \text{H}_2\text{O } \text{P} - \text{h } \text{H}_2\text{O } \text{R } \text{Q } \text{dot in b} = (\text{m } \text{dot}/\text{MM } \text{H}_2\text{O}^{\wedge} \text{Q in b } \text{PROPRIETARY MATERIAL. The energy balance for this system can be expressed as E } \text{Eout in } \text{Net energy transfer by heat, work, and mass Esystem } \text{Change in internal, kinetic, potential, etc. The fabric of those 16 chapters is greater than sufficient for an academic-year undergraduate course, and discretion, conditioned by the content material of different programs, is required within the selection of what's lined. 1-2C On a downhill road the potential energy of the bicyclist is being converted to kinetic energy, and thus the bicyclist picks up speed. 14- 1-7C There is no acceleration, thus the net force is zero in both cases. Analysis We take the entire contents of the tank, water + copper block, as the system. Properties The gas constant of nitrogen is $R = 0.2968 \text{ kJ/kg}\cdot\text{K}$. Analysis (a) For this problem, we use the properties from EES software. Nevertheless, a very powerful purposes of these legal guidelines, and the supplies and processes of biggest concern, differ from one department of science or engineering to one other. Limited distribution permitted only to teachers and educators for course preparation. The final results are to be plotted against the environment temperature. Therefore, this cannot happen. We'd additionally like to thank Professor Bharat Bhatt for his much-appreciated feedback and recommendation in the course of the accuracy verify. A scholar new to the topic will discover (that a) demanding job of discovery lies forward. Chemical-reaction equilibrium is roofed at size in Chap. From the air table (Table A-17) $\text{T1 } 290 \text{ K } \text{h1 } 29016 \text{. The purpose of a refrigerator is to remove heat from a refrigerated space whereas the purpose of an air-conditioner is remove heat from a living space. Analysis The expressions for the isentropic compression and expansion processes are } \text{T2 } \text{T1 } \text{r } (\text{k } 1) / \text{k } 1 \text{ T4 } \text{T3 } \text{rp } (\text{k } 1) / \text{k } 1 \text{ For an ideal regenerator, T5 T4 T qin } 5 4 2 1 \text{ T6 T } 2 3 6 \text{ qout } \text{s The thermal efficiency of the cycle is } \text{th } 1 \text{ q out TTT } (\text{T } / \text{T }) 1 1 6 1 1 1 6 1 \text{ q in T3 T5 T31 } (\text{T5 } / \text{T3 }) 1 \text{ T1 } (\text{T2 } / \text{T1 }) 1 \text{ T31 } (\text{T4 } / \text{T3 }) 1 (\text{k } 1) / \text{k } 1 \text{ T1 } \text{rp } (\text{k } 1) / \text{k } 1 \text{ T3 } \text{rp } (\text{k } 1) / \text{k } 1 \text{ For an ideal regenerator, T5 T4 T qin } 5 4 2 1 \text{ T6 T } 2 3 6 \text{ qout } \text{s The thermal efficiency of the cycle is } \text{th } 1 \text{ q out TTT } (\text{T } / \text{T }) 1 1 6 1 1 1 6 1 \text{ q in T3 T5 T31 } (\text{T5 } / \text{T3 }) 1 \text{ T1 } (\text{T2 } / \text{T1 }) 1 \text{ T31 } 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